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## INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

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<p>(21) International Application Number: PCT/KR98/00124 (22) International Filing Date: 19 May 1998 (19.05.98) (30) Priority Data: 1997/20056 22 May 1997 (22.05.97) KR (71) Applicant (for all designated States except US): DONAM SYSTEMS INC. [KR/KR]; 373-1, Kusong-dong, Yusong-gu, Taejon 305-701 (KR). (72) Inventors; and (75) Inventors/Applicants (for US only): KIM, Byoung, Yoon [KR/KR]; C-2 Daedong Village, Kung-dong, Yusong-gu, Taejon 305-335 (KR). KOH, Yeon, Wan [KR/KR]; 101-705 Hyundai Apartment, Doryong-dong, Yusong-gu, Taejon 305-340 (KR). KIM, Young, Kie [KR/KR]; 130-405 Hanbit Apartment, Uheun-dong, Yusong-gu, Taejon 130-405 (KR). YEO, Young, Bae [KR/KR]; 1199-49, Pyeongri 4-dong, Seo-gu, Taejon 703-014 (KR). (74) Agent: HUH, Jin, Seok; 206 Sungji Building, 1338-22, Seocho-dong, Seocho-ku, Seoul 137-070 (KR).</p>		<p>(81) Designated States: CN, JP, US, European patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE).  Published With international search report.</p>
<p>(54) Title: OPTICAL FIBER POLARIZATION CONTROLLER</p> <div data-bbox="363 1182 1110 1434" data-label="Image"> </div> <p>(57) Abstract</p> <p>An optical fiber polarization controller is disclosed which has compact size by employing wave plates made of short sections (110, 120) of a birefringent optical fiber. The optical fiber polarization controller controls the polarization state of input light by twisting or rotating birefringent slices (110, 120) connected to conventional single-mode fibers (100).</p>		

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## OPTICAL FIBER POLARIZATION CONTROLLER

### TECHNICAL FIELD

The present invention relates to an optical fiber polarization  
5 manipulating apparatus, more particularly to an optical fiber polarization  
controller which is very compact in size by using short pieces of  
birefringent fibers as waveplates.

### BACKGROUND ART

10 Light wave is an electromagnetic wave consisting of the electric  
and magnetic fields. As it propagates, the electric and magnetic fields  
oscillate on a transverse plane normal to the propagation direction with a  
specific oscillation pattern. In general, the polarization is a field which is  
parallel to the electric field vector  $E$ . Therefore, the state of polarization is  
15 referred to the oscillation pattern of the electric field on the transverse  
plane. The state of polarization falls into three categories in terms of the  
direction and phase of two mutually-orthogonal components of the electric  
field vectors  $E$ . The categories are linear, circular, and elliptical  
polarization, respectively.

20 The state of polarization is changed when light propagates through  
a birefringence medium which has different refractive-indices between two  
orthogonal eigen axes. The amount of birefringence, or the index  
difference, is the characteristics of the material itself, however it is affected  
by external perturbations such as stress, strain and temperature. Silica  
25 material is inherently birefringence-free because of its amorphous nature.  
However, optical fibers that are made of silica tend to exhibit non-

negligible birefringence owing to the internal stress as well as non circular-symmetric geometry. Additional birefringence can be also induced by external lateral stress or bending. The change of such birefringence by external perturbations which is often non-deterministic can cause severe problems in fiber-optic applications such as optical communications and sensors. The effects include polarization-induced signal fading or degradation due to the change of polarization state. It is therefore very important in fiber-optic applications to maintain or control the polarization state of light. A polarization controller is an apparatus used to convert an input polarization state to an arbitrary output polarization state and, therefore, a key element in lab experiments, fiber-optic sensors, optical communications, and especially for a system which uses highly polarization dependent optical devices. For example, high-speed optical system employs lithium niobate( $\text{LiNbO}_3$ ) as an external modulator to reduce wavelength chirping that comes in at directly modulated light source. In this case, due to the high-polarization dependence of the modulator, matching the polarization state to the birefringence axis of the modulator is essential to get the best performance. In matching the polarization state between a laser diode("LD") and the external modulator, polarization maintaining("PM") fiber is generally used to connect the LD to the external modulator. However, this requires complex process of aligning polarization axis of fiber to those of the LD and the external modulator.

The principle of the polarization controller is that desired polarization state is obtained by using appropriate phase retarders which can transform a state of polarization("SOP") to another SOP. Two quarter-

wave plates can be used for the phase retarders.

FIG. 1 illustrates the change of SOP on Poincare Sphere which is generally accepted way to describe the SOP. The convention is that a linear polarization state can be represented by a point "c" located on the equator, and circular polarization by a point "d" located on the pole of the Poincare sphere. A point on the sphere corresponds to a SOP. Since two orthogonal axes of a coordinates can describe any point on the sphere, a point on the sphere can be moved to another point by rotating the two orthogonal axes of the coordinate. This means that any SOP of light can be transformed to any other SOP by means of rotating the axes. It is well-known that two quarter-wave plates that are used in a polarization controller, for example bent fiber loops for making phase retardation by inducing birefringence therein, can perform the above described two rotating axes.

When two quarter-wave plates are used for a polarization controller, the respective azimuthal and polar angles of a point on the sphere can be rotated by rotating two axes of the sphere, namely, the optical axes of two quarter-wave plates. Therefore, input SOP "a" can be transformed to a desired output SOP "b" as shown in FIG. 1.

FIG. 2 schematically shows a conventional optical fiber polarization controller according to a prior art.

The polarization controller shown in FIG. 2 is disclosed by H. C. LeFevre, in Electronics Letters, Vol. 16, No. 20, September 1980. Referring to FIG. 2, a length of single mode optical fiber 1 is wound on a bobbin 10 with a predetermined diameter. The bending gives birefringence to the optical fiber by bending-induced stress, which makes two

birefringence axes, parallel and perpendicular to bobbin 10. At an appropriate diameter, the induced birefringence makes a quarter-wave plate for a given optical wavelength. Since the birefringence principal axis rotates as the rotation of bobbin 10 to R-direction, the SOP of input light  $P_{in}$  can be controlled to a desired SOP polarization state in output light  $P_{out}$ . With this bobbin, the polarization controller can not avoid comparably large volume, making it hard to be mounted on a common circuit board.

FIG. 3 is a cross sectional view showing the application of other polarization controller of prior arts. This kind of polarization controller can give small size compared with the above described prior art. Referring to FIG. 3, the polarization controller has a screw 32 which can contact the outer surface of optical fiber 31. In the polarization controller of FIG. 3, the polarization state is controlled by the birefringence, induced from the mechanical stress which is applied to the optical fiber by screw 32. In principle, there should be means for acting as two orthogonal rotating axes to control the polarization state as described in FIG. 1. The means to achieve this action is the screw that presses the optical fiber from different directions with different force, which corresponds to the two orthogonal axes of the above polarization controller. For example, as shown in FIG. 3, after the stress applied in X-Y direction is released, other stress is applied in X'-Y' direction. This single controlling means may cause difficulty in controlling the polarization. The problem with such polarization controller is that the reliability of the polarization controller is significantly affected by the squeezing of the fiber, because the squeezing can damage the jacket of the fiber and fiber itself. Moreover, the mechanically squeezed jacket may not recover its original form so that the stress still remains in the fiber,

which results in uncontrollable situation.

## DISCLOSURE OF INVENTION

It is therefore an object of the present invention to provide an  
5 optical fiber polarization controller with meaningfully small size  
applicable to an electric circuit board.

It is other object of the present invention to provide an optical fiber  
polarization controller having improved durability without squeezing the  
optical fiber.

10 It is another object of the present invention to provide an  
inexpensive optical fiber polarization controller without using PM optical  
fiber for entire fiber strand of the controller.

In order to accomplish the aforementioned object, the present  
invention provides an optical fiber polarization controller, comprising: at  
15 least one part of a first optical fiber having birefringence, a part of a  
second single-mode optical fiber having at least one connected point with  
the first optical fiber to the end of the part to form a strand of optical fibers  
for transmitting light along the strand; and a twisting means for controlling  
angle of the birefringence axes of the first fiber.

20 The connected points can be formed by fusion splicing and/or  
physical contact. The optical fiber polarization controller may be  
configured to have more than two parts of the first optical fiber.

Each of the parts may have a length adjusted to perform a quarter  
wave plate according to the difference between its birefringence indices.

25 According to other aspect of the invention, the optical fiber  
polarization controller comprises: two slices of a first optical fiber having



birefringence; two parts of a second single-mode optical fiber, each part having a connected portion to the end of the slice to transmit light with the slices; a pair of ferrules for inserting the connected portions and the slices therein, and for aligning two parts of the first single-mode optical fiber by  
5 contacting the facing ends of two slices; a sleeve for inserting the pair of ferrules to fix it therein; and a rotating means for ferrules.

The connected portions may also be formed by fusion splicing or physical contact. Each of the slices can have a length adjusted to perform a quarter-wave plate according to the difference between its birefringence  
10 indices.

The structure of the connected portions is not limited to the aforementioned structure, and any structure can be used if low connection losses are guaranteed.

## 15                   **BRIEF DESCRIPTION OF DRAWINGS**

FIG. 1 illustrates the change of polarization state on Poincare Sphere which is frequently used to show the polarization state of light;

FIG. 2 schematically shows a conventional optical fiber  
20 polarization controller according to a prior art;

FIG. 3 is a cross sectional view showing the application of other polarization controller of prior arts;

FIG. 4 is a partially enlarged view showing only optical fibers in the optical fiber polarization controller according to an embodiment of the  
25 invention;

FIG. 5 shows other embodiment of the invention with a more

compact size than the one in FIG. 4;

FIG. 6(a) to FIG. 6(c) schematically show a fixing apparatus to mount the optical fiber part of the optical fiber polarization controller on a electric circuit board.

5

### BEST MODE FOR CARRYING OUT THE INVENTION

Hereinafter, preferred embodiments of the present invention will be described referring to the accompanying drawings.

FIG. 4 is a partially enlarged view showing only optical fibers in the in-line optical fiber polarization controller according to an embodiment of the invention.

Referring to FIG. 4, the end portions "f" of slices 110 and 120 are optically connected to the second optical fiber 100 to form a strand of optical fibers capable of transmitting light. The slices 110 and 120 of the first optical fiber are birefringent, that is, have two birefringent axes of different refractive indices from each other. A conventional single mode fiber with low birefringence can be used as the second optical fiber 100. The connection between the second optical fibers 100 and slices 110 and 120 can be made by fusion splicing. Other connecting method includes mechanical splicing or physical contact aided by a ferrule. Slices 110 and 120 are short sections of a birefringent optical fiber with proper length to perform the function of wave plates. Typically, the length can be adjusted to act as a quarter-wave plate or half-wave plate. For example, when the index difference( $\Delta n$ ) between the birefringence axes of the slices is an order of  $10^{-4}$  as in this embodiment, the length of the slices 110 and 120 would be only a few mm's for an optical wavelength of about 1.5

micrometer. When an optical wave with a certain polarization state transmits through single or multiple birefringent slices, the output polarization state is determined by the settings of the birefringence axes of the slices with respect to each other and also to the input polarization state.

5 Therefore, by rotating the birefringence axes, any polarization state in the input light can be transformed to any polarization state in the output. To do this, one can rotate the slice with respect to the birefringent slices spliced to them. If the slices are mechanically connected to the lead fiber by using a ferrule, the slices can be rotated with respect to the lead fibers to change  
10 the orientation of the birefringence axes. Other means includes lateral stress applied to the slices to change the magnitude of the birefringence.

FIG. 5 shows other embodiment of the invention with a more compact size than the one in FIG. 4. The piece of the second optical fiber between the optical fiber slices 110 and 120 shown in FIG. 4 is not  
15 necessary. In this embodiment, two slices of the birefringent first optical fiber, 502 and 504, are connected to pieces 500 of the second single mode optical fiber by fusion splicing. Then, the yet free ends of the slices 502 and 504 are connected to each other by a mechanical splicing or physical contact. For ease of this splicing process, conventional physical contact  
20 based on ferrules and sleeves can be used. Specifically, the slices 502 and 504 are inserted into ferrules 506 and 508, respectively. The ferrules 506 and 508 are aligned to each other for minimum optical loss with help of a cylindrical sleeve 510. The material for ferrules 506 and 508 was zirconia in this particular embodiment, however could be stainless steel, quartz,  
25 alumina, or the like. The first optical fiber slices 502 and 504 are physically contacted without using fusion splicing. The typical optical loss

of the physical contact could be less than 0.2 dB.

FIG. 6(a), 6(b) and 6(c) schematically show a fixing apparatus from different angles which is used to mount the optical fiber elements of the optical fiber polarization controller. FIG. 6(a) is a side view, FIG. 6(b) is a  
5 plane view and FIG. 6(c) is a front view of the assembled apparatus. A strand of optical fiber composed of the first optical fiber slices 110, 120 and the second optical fiber 100 of FIG.4 passes lengthwise through a hollow cylindrical fixing apparatus 40. Knobs are used to fix the position of the cylindrical fixing apparatus 40. Also, the knobs help the process of  
10 rotating and fixing at a position of the cylindrical fixing apparatus. The above described fixing apparatus can be miniaturized to a size small enough to be mounted on a electric circuit board.

The performance of the optical fiber polarization controller manufactured as above was analyzed. Total insertion loss of the  
15 polarization controller was less than 0.5 dB, and the back reflection was far below -60dB. Arbitrary input polarization state could be transformed to any output polarization state with an excellent polarization extinction of greater than -45dB. Moreover, since the second optical fiber was a conventional communication grade single-mode optical fiber, the  
20 polarization controller is perfectly compatible with other fiber-optic components and instruments through fusion splicing or conventional connectors. Unlike the prior arts that was comprised of an apparatus for bending optical fibers to induce birefringence, the polarization controller according to the invention is much more compact in size. Further, the  
25 polarization controller according to the invention is more durable than another prior art in which an optical fiber has to be squeezed laterally with

frequency changes of the magnitude and direction of the squeezing. Moreover, the polarization controller according to the invention provides inexpensive optical communication systems since entire strand of the optical fibers is composed of common communication grade optical fibers  
5 instead of polarization maintaining optical fibers.

**WHAT IS CLAIMED IS :**

## 1. An apparatus comprising:

a section of a first optical waveguide with birefringence axes of  
5 different refractive indices;

a second optical waveguide connected to said section of the first  
optical waveguide to transmit light from the second optical waveguide to  
the first optical waveguide, or from the first optical waveguide to the  
second optical waveguide; and

10 a controlling means to rotate the birefringence axes of said section  
of the first optical waveguide with respect to said second optical  
waveguide;

wherein said section of the first optical waveguide is sized to  
provide phase delay equal to single or a multiple of quarter  $\pi(\pi)$  radian  
15 between two eigen polarization states defined by the birefringence axes.

2. The apparatus of claim 1, wherein the first optical waveguide  
includes polarization maintaining optical fiber.

3. The apparatus of claim 1, wherein the connection between said  
section of the first optical waveguide and the second optical waveguide is  
20 made by fusion splicing or physical contact.

4. The apparatus of claim 3, wherein said controlling means  
includes a twisting means for applying twist to the second optical  
waveguide.

## 5. An apparatus comprising:

25 a plurality of sections of a first optical waveguide with  
birefringence axes of different refractive indices;

a plurality of sections of a second optical waveguide connected to said sections of the first optical waveguide to transmit light from the second optical waveguide to the first optical waveguide, or from the first optical waveguide to the second optical waveguide; and

- 5 a controlling means to rotate the birefringence axes of said sections of the first optical waveguide with respect to adjacent sections of the second optical waveguide;

wherein said sections of the first optical waveguide are sized to provide phase delay equal to single or a multiple of quarter  $\pi$  ( $\pi$ ) radian  
10 between two eigen polarization states defined by the birefringence axes.

6. The apparatus of claim 5, wherein the first optical waveguide includes polarization maintaining optical fiber.

7. The apparatus of claim 5, wherein the connection between said sections of the first optical waveguide and the second optical waveguide is  
15 made by fusion splicing or physical contact.

8. The apparatus of claim 7, wherein said controlling means includes a twisting means for applying twist to said sections of the second optical waveguide.

9. An apparatus comprising:

20 a plurality of sections of a first optical waveguide with birefringence axes of different refractive indices;

a plurality of sections of a second optical waveguide,

wherein at least one of said sections of the first optical waveguide is connected to each other and the rest of said sections of the first optical  
25 waveguide is connected to said sections of the second optical waveguide;

and a controlling means to rotate the birefringence axes of said

sections of the first optical waveguide;

wherein said sections of the first optical waveguide are sized to provide phase delay equal to single or a multiple of quarter  $\pi(\pi)$  radian between two eigen polarization states defined by the birefringence axes.

5        10. The apparatus of claim 9, wherein the first optical waveguide includes polarization maintaining optical fiber.

11. The apparatus of claim 9, wherein the connection between said sections of the first optical waveguide and the second optical waveguide is made by fusion splicing or physical contact.

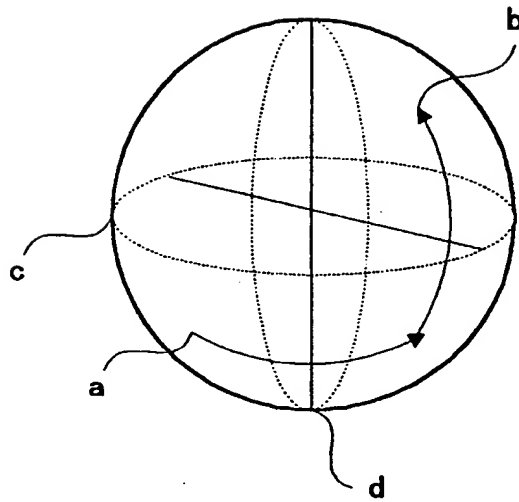
10        12. The apparatus of claim 9, wherein the connection between said sections of the first optical waveguide is made by physical contact.

13. The apparatus of claim 12, wherein the physical contact is aided by ferrules and sleeves.

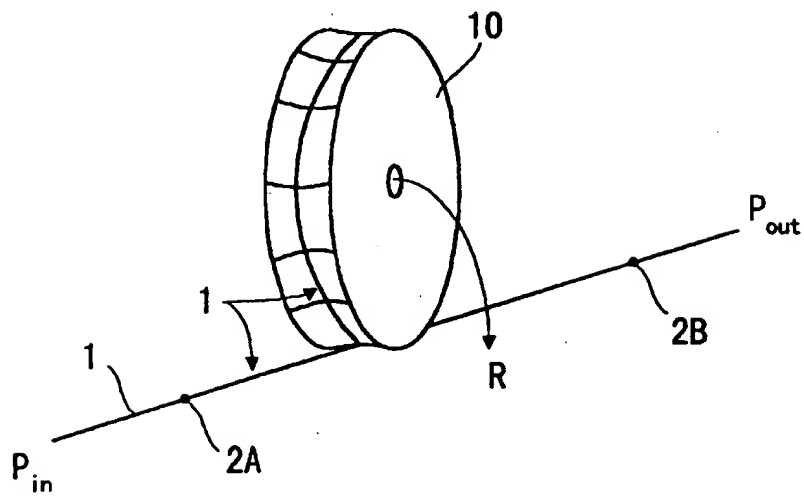
15        14. The apparatus of claim 9, wherein said controlling means includes a twisting means for applying twist to said sections of the second optical waveguide.

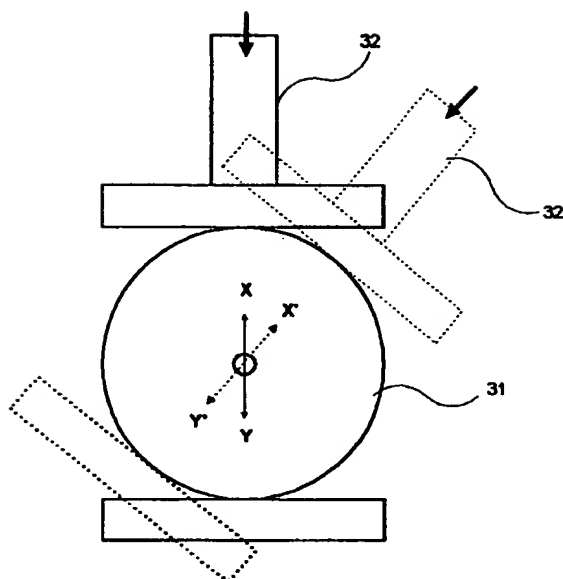
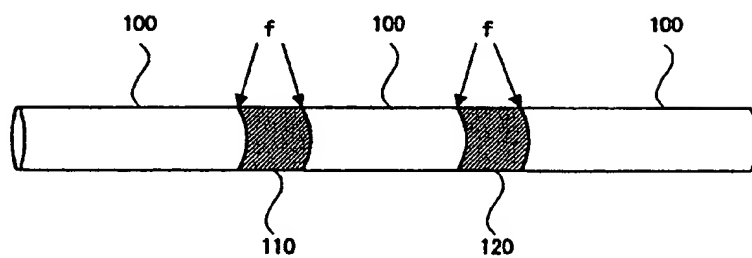


**FIG. 1**

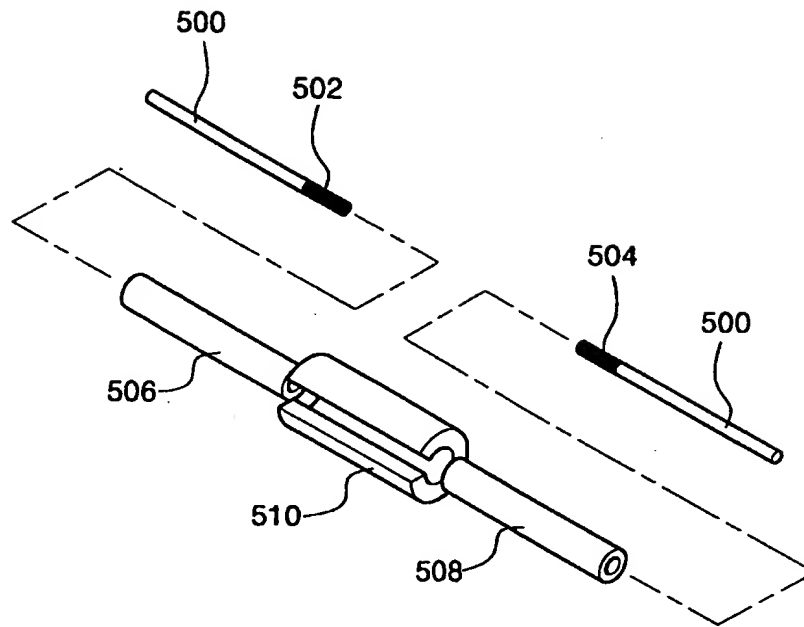
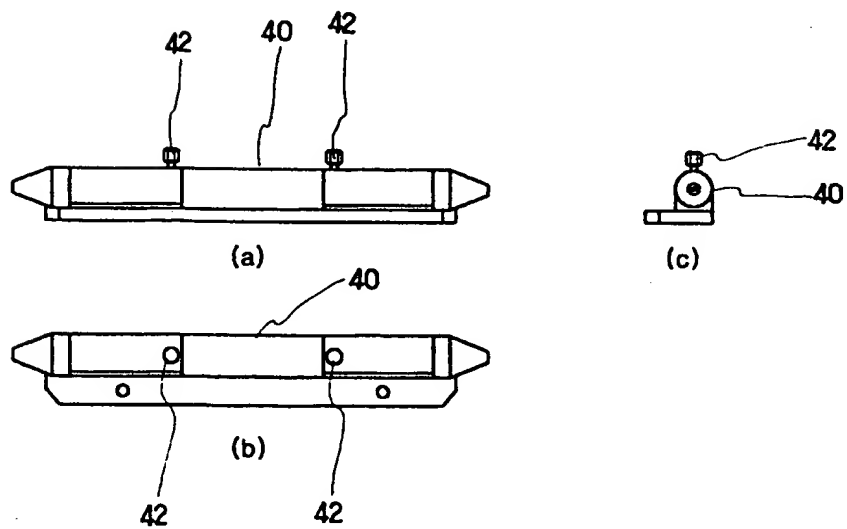


**FIG. 2**



**FIG. 3****FIG. 4**

3/3

**FIG. 5****FIG. 6**

# INTERNATIONAL SEARCH REPORT

International application No.

PCT/KR 98/00124

## A. CLASSIFICATION OF SUBJECT MATTER

IPC<sup>6</sup>: G 02 B 6/27, 6/10; G 02 F 1/01

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## B. FIELDS SEARCHED

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Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

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EPODOC, WPI, PAJ

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

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A	US 5 457 756 A (HARTL et al.) 10 October 1995 (10.10.95), column 1, line 7 - column 2, line 57; column 3, lines 43-67; fig. 1-3.	1-3,5-7,9-13
A	US 4 603 941 A (FUJII et al.) 05 August 1986 (05.08.86), column 1, line 54 - column 2, line 19; fig. 6,8.	1-4
A	Patent Abstracts of Japan, vol. 7, no. 127 (P-201), 1983, JP 58-046310 A (NIPPON).	1-4
A	EP 0 386 790 A2 (NEC CORPORATION) 12 September 1990 (12.09.90), abstract; fig. 1-4.	1,5,9

☐ Further documents are listed in the continuation of Box C.

☒ See patent family annex.

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